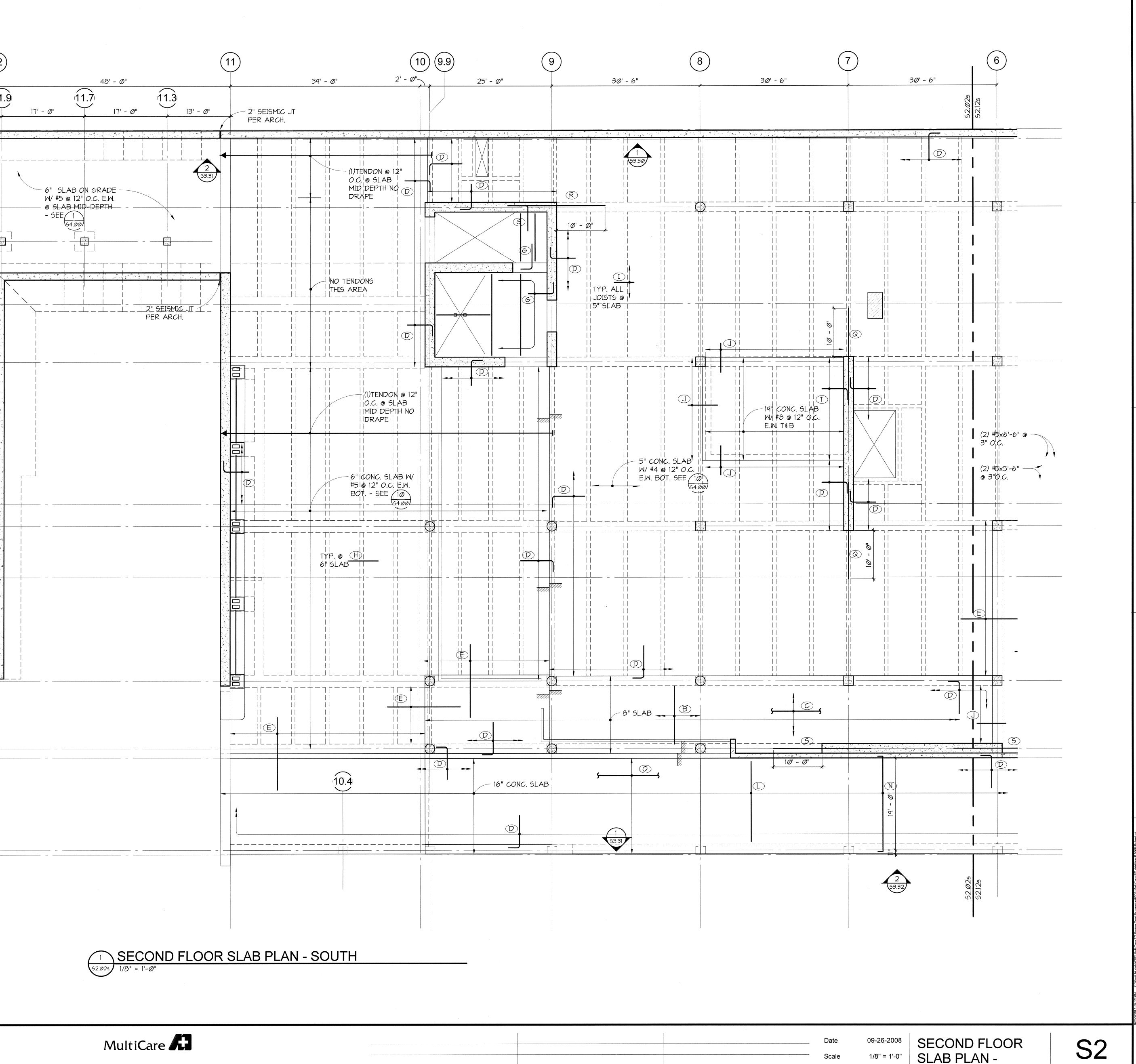
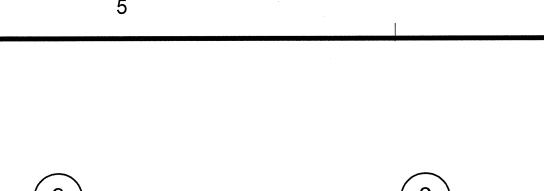
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<u>NOTE</u>	<u>S</u> .			
	SEE SHEET S4.10 FOR TYPICAL POS DETAILS AND SCHEDULES.		(D.1)	
2. 3.	INDICATES POUR-STRIP, C 56 DAYS AFTER FINAL DE SEE SHEET S3.50 FOR COLUMN SCH	ECK.		
4.	SEE 55.50 FOR TYPICAL CMU WALL	DETAILS.		
5. 6.	SEE 54.20 FOR TYPICAL CONCRET INDICATES C.G.S OF POST-T CONTROL POINT MEASURED	ENSIONING TENDONS AT	(C.7)	
٦.	TYPICAL. SEE DETAIL 1/S4.11 CONTROL POINTS. TYPICAL SLAB POST-TENSIONING F	FOR TYPICAL LAYOUT OF		
	= 1.5" AT SLAB MID-SPAN U.N. = 7" CENTERED OVER SUPPOR	О.	21' - 5" - 5"	
			1	
	SECOND FLOOR SLAB R	EINFORCING SCHEDULE	C	
MARK	< CALLOUT	EINFORCING SCHEDULE REMARKS		
A B			(B.1)	
A B C D	< CALLOUT #6x16'-Ø" @ 12" O.C. BOT. #5x12'-Ø" @ 12" O.C. BOT. #5 @ 12" O.C. ALT. TOP & BOT. 5'-2" #5 @ 6" O.C. TOP			
A B C	< CALLOUT #6x16'-Ø" @ 12" O.C. BOT. #5x12'-Ø" @ 12" O.C. BOT. #5 @ 12" O.C. ALT. TOP & BOT. 5'-2" #5 @ 6" O.C. TOP #5x15'-Ø" @ 12" O.C. TOP #6x23'-Ø" @ 12" O.C. BOT.		B.1 B.1 B.1 B.1 B.1	
 A B C D E 	< CALLOUT #6x16'-Ø" @ 12" O.C. BOT. #5x12'-Ø" @ 12" O.C. BOT. #5 @ 12" O.C. ALT. TOP & BOT. 5'-2" #5 @ 6" O.C. TOP #5x15'-Ø" @ 12" O.C. TOP #6x23'-Ø" @ 12" O.C. BOT. 5'-2" #5 @ 012" O.C.		B.1 (B.1)	
	< CALLOUT #6x16'-Ø" @ 12" O.C. BOT. #5x12'-Ø" @ 12" O.C. BOT. #5 @ 12" O.C. ALT. TOP & BOT. 5'-2" #5 @ 6" O.C. TOP #5x15'-Ø" @ 12" O.C. TOP #6x23'-Ø" @ 12" O.C. BOT. 5'-2" #5 @ 12" O.C. TOP #4x4'-Ø" @ 12" O.C. TOP #5x6'-Ø" @ 12" O.C. TOP		B.1 B.1 B.1 B.1 B.1 B.1 B.1 B.1 B.1 B.1	
$ \begin{array}{ c c } \hline A \\ \hline B \\ \hline C \\ \hline D \\ \hline E \\ \hline F \\ \hline G \\ \hline \hline 1 \\ \hline \end{bmatrix} \\ \hline K \\ \hline \\ \hline \end{bmatrix} $	< CALLOUT # $6 \times 16' - 0" @ 12" O.C. BOT.$ # $5 \times 12' - 0" @ 12" O.C. BOT.$ # $5 @ 12" O.C. ALT. TOP & BOT.$ 5' - 2" # $5 @ 6" O.C. TOP$ # $5 \times 15' - 0" @ 12" O.C. TOP$ # $6 \times 23' - 0" @ 12" O.C. BOT.$ 5' - 2" # $5 @ 12" O.C. TOP$ # $4 \times 4' - 0" @ 12" O.C. TOP$ # $4 \times 4' - 0" @ 12" O.C. TOP$ # $5 \times 6' - 0" @ 12" O.C. TOP$ (5) # $9 \times 12' - 0" @ 3" O.C.$ # $10 @ 8" O.C. BOT.$		$B = \frac{1}{100} - $	
	< CALLOUT #6x16'- \emptyset " @ 12" O.C. BOT. #5x12'- \emptyset " @ 12" O.C. BOT. #5 @ 12" O.C. ALT. TOP & BOT. 5'-2" #5 @ 6" O.C. TOP #5x15'- \emptyset " @ 12" O.C. TOP #6x23'- \emptyset " @ 12" O.C. BOT. 5'-2" #5 @ 12" O.C. TOP #4x4'- \emptyset " @ 12" O.C. TOP #4x4'- \emptyset " @ 12" O.C. TOP #5x6'- \emptyset " @ 12" O.C. TOP (5) #9x12'- \emptyset " @ 3" O.C. #10 @ 8" O.C. BOT. #4x9'- \emptyset " @ 12" O.C. BOT. #4 @ 12" O.C. TOP		$\begin{bmatrix} \mathbf{B}, 1 \\ \mathbf{B} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\$	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	CALLOUT # $6 \times 16' - 0'' @ 12'' O.C. BOT.$ # $5 \times 12' - 0'' @ 12'' O.C. BOT.$ # $5 @ 12'' O.C. ALT. TOP & BOT.$ $5' - 2'''$ # $5 @ 0'' O.C. ALT. TOP & BOT.$ $5' - 2''''$ # $5 @ 0'' O.C. ALT. TOP & BOT.$ $5' - 2''''''' @ 0'' O.C. TOP$ # $5 \times 15' - 0'' @ 12'' O.C. TOP$ # $5 \times 2^{3'} - 0'' @ 12'' O.C. BOT.$ $5' - 2''''''' @ 12'' O.C. TOP$ # $5 @ 12'' O.C. TOP$ # $5 @ 12'' O.C. TOP$ # $5 @ 12'' O.C. TOP$ # $4 \times 4' - 0'' @ 12'' O.C. TOP$ # $5 \times 6' - 0'' @ 12'' O.C. BOT.$ # $10 @ 0'' O.C. BOT.$ # $4 \times 9' - 0'' @ 12'' O.C. BOT.$ # $4 @ 12'' O.C. TOP$ # $10 @ 0'' O.C. TOP$ # $10 @ 0'' O.C. TOP$		$\begin{bmatrix} \mathbf{B}, 1 \\ \mathbf{B} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\$	
	< CALLOUT # $6x16'-0" @ 12" O.C. BOT.$ # $5x12'-0" @ 12" O.C. BOT.$ # $5 @ 12" O.C. ALT. TOP & BOT.$ 5'-2" # $5 @ 0" O.C. TOP$ # $5x15'-0" @ 12" O.C. TOP$ # $6x23'-0" @ 12" O.C. BOT.$ 5'-2" # $5 @ 12" O.C. TOP$ # $4x4'-0" @ 12" O.C. TOP$ # $4x4'-0" @ 12" O.C. TOP$ # $4x4'-0" @ 12" O.C. TOP$ (5) # $9x12'-0" @ 3" O.C.$ # $10 @ 0" O.C. BOT.$ # $4x9'-0" @ 12" O.C. BOT.$ # $4x9'-0" @ 12" O.C. BOT.$ # $4 @ 12" O.C. TOP$ # $4 @ 12" O.C. TOP$ # $4 @ 12" O.C. TOP$ (2) # $9x20'-0" @ 3" O.C.$ (6) # $10x20'-0" @ 3" O.C.$		$\begin{bmatrix} \mathbf{B}, 1 \\ \mathbf{B} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\$	
	<pre>< CALLOUT #$6x16'-0" @ 12" O.C. BOT.$ #$5x12'-0" @ 12" O.C. BOT.$ #$5 @ 12" O.C. ALT. TOP & BOT.$ 5'-2" #$5 @ 0" O.C. TOP$ #$5x15'-0" @ 12" O.C. TOP$ #$6x23'-0" @ 12" O.C. BOT.$ 5'-2" #$5 @ 0.C. TOP$ #$4x4'-0" @ 12" O.C. TOP$ #$4x4'-0" @ 12" O.C. TOP$ #$4x4'-0" @ 12" O.C. TOP$ (5) #$9x12'-0" @ 3" O.C.$ #$10 @ 0" O.C. BOT.$ #$4x9'-0" @ 12" O.C. BOT.$ #$4x9'-0" @ 12" O.C. BOT.$ #$4x9'-0" @ 12" O.C. BOT.$ #$4x9'-0" @ 12" O.C. TOP$ #$4x9'-0" @ 12" O.C. TOP$ #$4 @ 12" O.C. TOP$ (2) #9x20'-0" @ 3" O.C.</pre>		$\begin{bmatrix} \mathbf{B}, 1 \\ \mathbf{B} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\$	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	 		$\begin{bmatrix} \mathbf{B}, 1 \\ \mathbf{B} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\$	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		$\begin{bmatrix} \mathbf{B}, 1 \\ \mathbf{B} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\ \mathbf{C} \\ \mathbf{B} \\ \mathbf{C} \\$	



ENCY DEPARTMENT & CANCER CENTER EXPANSION

TACOMA, WASHINGTON





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